

# Modified Level II Streambed-Scour Analysis for Structure I-465-131-5256 Crossing Williams Creek in Hamilton County, Indiana

By BRET A. ROBINSON, DAVID C. VOELKER,  
and ROBERT L. MILLER

Prepared in cooperation with the  
INDIANA DEPARTMENT OF TRANSPORTATION

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BRUCE BABBITT, Secretary

U.S. GEOLOGICAL SURVEY  
Gordon P. Eaton, Director

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For additional information, write to:  
District Chief  
U.S. Geological Survey  
Water Resources Division  
5957 Lakeside Boulevard  
Indianapolis, IN 46278-1996

Copies of this report can be purchased from:  
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## CONVERSION FACTORS AND ABBREVIATIONS

<b>Multiply</b>	<b>By</b>	<b>To obtain</b>
inch (in.)	25.4	millimeter
foot (ft)	0.3048	meter
square foot (ft <sup>2</sup> )	929.0	square centimeter
feet per second (ft/s)	0.3048	meters per second
cubic foot per second (ft <sup>3</sup> /s)	0.02832	cubic meter per second
mile (mi)	1.609	kilometer
square mile (mi <sup>2</sup> )	2.590	square kilometer

### Abbreviations used in this report:

D <sub>50</sub>	median diameter of bed material
Q100	100-year discharge
FEMA	Federal Emergency Management Agency
HEC	Hydraulic Engineering Circular
IDNR	Indiana Department of Natural Resources
INDOT	Indiana Department of Transportation
USGS	U. S. Geological Survey
WSPRO	Water Surface PROfile model

# Modified Level II Streambed-Scour Analysis for Structure I-465-131-5256 Crossing Williams Creek in Hamilton County, Indiana

By Bret A. Robinson, David C. Voelker, *and* Robert L. Miller

## ABSTRACT

Level II scour evaluations follow a process in which hydrologic, hydraulic, and sediment-transport data are evaluated to calculate the depth of scour that may result when a given discharge is routed through a bridge opening. The results of the modified Level II analysis for structure I-465-131-5256 on Interstate 465 crossing Williams Creek in Hamilton County, Indiana, are presented. The site is near the city of Indianapolis and is in the southwestern part of Hamilton County. Scour depths were computed with the Water Surface PROfile model, version V050196, which incorporates the scour-calculation procedures outlined in Hydraulic Engineering Circular No. 18. Total scour depths at the piers were approximately 6.5 feet for the modeled discharge of 4,300 cubic feet per second and approximately 9.8 feet for the modeled discharge of 7,310 cubic feet per second.

## INTRODUCTION

The U.S. Geological Survey (USGS), in cooperation with the Indiana Department of Transportation (INDOT), is conducting Level II scour analyses at a number of bridges throughout Indiana. This report describes the methods applied and the modeling results for bridge I-465-131-5256.

## Background and Scope

Level I scour assessment is a process where a large number of bridges are studied as a group. Assessments usually are made by evaluating a combination of geomorphic, hydrologic, and bridge-characteristic data. The results help investigators determine which bridges appear to be most likely to experience streambed-scour problems and which bridges appear to be relatively immune to problems brought on by streambed scour (for example, bridges built on bedrock).

When applied correctly, Level I scour assessments provide an investigator with information to identify those bridges that appear to be relatively safe and those bridges that fall into higher risk categories.

Level II scour evaluations describe the process for an investigator to apply a model to a bridge site and calculate the potential depth of scour that may result from a given flood event. Level II analyses involve the application of basic hydrologic, hydraulic, and sediment-transport engineering concepts and may include an evaluation of flood history, channel hydraulic conditions (for example, water-surface profile analysis), and basic sediment-transport analyses such as scour calculations (Lagasse and others, 1995).

The methods and model outlined in Hydraulic Engineering Circular (HEC) No. 18 (Richardson and Davis, 1995) formulate the basis for Level II scour evaluations. Methods used in this study for Level II scour evaluations are a modification of the HEC-18 standards. These modifications were made to comply with the methodology requested by INDOT (Merril Dougherty, Indiana Department of Transportation, oral commun., 1996). Descriptions of the specific modifications are given in the "Evaluation Methods" section of this report.

This report presents the methods followed for modeling, special considerations for this study site, and the input for and the output from the Water Surface PROfile (WSPRO) model.

### **Site Description**

The study site is located near the city of Indianapolis and is in the southwestern part of Hamilton County. The drainage area for the site is approximately 16.9 mi<sup>2</sup> (Merril Dougherty, Indiana Department of Transportation, written commun., 1997). The predominant land use in the basin is urban; in the immediate vicinity of the bridge, the land is predominantly brush covered with some suburban areas nearby.

Within the immediate vicinity of the bridge, Williams Creek has a channel-bed slope of approximately 0.0025 ft/ft. The channel-bed material is gravelly sandy silt-clay, and the channel banks consist of sandy silt-clay. At the time of the Level I site visit on August 3, 1994, the banks were observed to have 0 to 50 percent woody vegetative cover; the field report noted that the banks were experiencing some fluvial erosion.

The Interstate 465 crossing of Williams Creek is a 111-ft-long, multi-lane bridge consisting of three spans supported by concrete and steel piers and sloping spill-through abutments. Additional details describing conditions at the site are included in the Level I data base (Hopkins and Robinson, unpub. data, 1997). Photographs of the site, taken at the time of the Level I site visit, are archived at the USGS office in Indianapolis.

## EVALUATION METHODS

The methods described in this section apply to a number of bridge sites in Indiana being evaluated for scour and outline the procedures requested by INDOT for these modified Level II scour analyses. The principal modification requested by INDOT was that the input data to the model come from or be estimated from existing data sources; no additional field data were collected. Actual methods used in the scour evaluation at this particular bridge site use the most applicable method possible, given the data available.

To determine drainage area, either published values found in Hoggatt (1975) or USGS 7.5-minute topographic maps with Hoggatt's original drainage-area delineations were used. Where there are no published data, drainage-area segments measured from the maps produced by Hoggatt were either subtracted from downstream sites or added to upstream sites published by Hoggatt (1975).

In Indiana, flood discharges are coordinated by agreement among State and Federal agencies. At sites where flood discharges officially are coordinated among State and Federal agencies in Indiana, the coordinated 100-year discharge (Q100) was modeled. INDOT also provided an additional flood discharge for these coordinated sites in excess of the Q100 to be modeled.

If a flood discharge was not coordinated, the USGS examined Federal Emergency Management Agency (FEMA) studies for Q100 determinations. Where FEMA studies did not produce a Q100, the USGS contacted IDNR for an estimated Q100 in the vicinity of the site being studied. If IDNR did not have a Q100, data from nearby USGS streamflow-gaging stations were analyzed with nearby and similar drainage basins that have been coordinated. At sites having no coordinated discharge data, the two discharges used in the model were 1) the approximated Q100 and 2) a discharge equal to 1.7 times the approximated Q100.

Most of the cross-section and bridge-opening geometry data were taken from the bridge plans (Indiana State Highway Commission, 1965) provided by INDOT. Bridge plans are presumed to be representative of current conditions at the site. To determine the cross-section geometry, a line was drawn on the bridge plans parallel to the bridge stationing and approximately one bridge width from the bridge. For sites where the bridge plans did not extend far enough laterally for collection of all cross-section data required for WSPRO model analysis, additional data were collected from 7.5-minute topographic maps.

The roadway and embankment profile was taken from the bridge and highway plans for those sites where roadway overtopping was expected. The INDOT bridge plans and 7.5-minute topographic maps were used as a guide, based on the water-surface elevations calculated by the WSPRO model, to determine if roadway overtopping might occur.

Roughness values (*n*-values) for the main channel were estimated by viewing photographs archived from the Level I scour assessments. The *n*-values for the overbanks were assigned on the basis of the surface-cover data summarized in the Level I data base (Hopkins and Robinson, unpub. data, 1997). From those data, the following roughness values were assigned to the surface-cover categories: urban—0.050, suburban—0.035, row crop—0.045, pasture—0.035, brush—0.120, forest—0.100, and wetland (any area covered by standing water)—0.100. The *n*-values for the overbanks were adjusted if the Level I photographs provided sufficient detail to warrant an adjustment.

WSPRO version V050196 was used to model flow through the study site. Starting water-surface elevation was obtained with a slope-conveyance computation. The channel-bed slope in the immediate vicinity of the bridge was estimated from the 7.5-minute topographic map and was used as the slope of the energy grade line for this computation.

WSPRO version V050196 includes a field that allows the input of up to four scour-adjustment factors (K1 to K4). For this modeling, the default value for K4 (bed armoring) was chosen. For scour-adjustment factors K1 and K2 (pier-nose shape and angle of attack, respectively), input values were determined by evaluating the data archived in the Level I data base (Hopkins and Robinson, unpub. data, 1997). For the K3 factor (bed forms), a value of 1.1 was applied in all cases.

In some cases, piers set on the overbanks are constructed with footings that are higher in elevation than pier footings in the main channel. In these situations, if the channel position changes, the piers that were initially constructed on the overbank may become part of the main channel. Therefore, to evaluate total potential scour, the model results obtained for contraction scour and deepest local scour in the main channel were added and applied to all piers in the bridge opening. This methodology allowed for an evaluation of potential undermining of pier supports in the event that future channel movement placed overbank piers in the main channel.

Where bridge pairs have a continuous abutment or fill between the bridges that does not allow expansion of flow, the bridge pair was modeled as one bridge. Sites with discontinuous abutments, allowing expansion between the bridges, were modeled as two separate bridges. In those cases, a valley cross section was measured between the bridges and used as the approach section for the downstream bridge and as the exit section for the upstream bridge.

At sites with no embankment to function as a weir or at sites where the tailwater drowns out the embankment, a composite bridge and road section was used to compute flow. Those sites were computed with friction-loss equations rather than with a bridge routine.

Total scour is taken as the sum of local scour plus contraction scour. If the model predicted negative contraction scour (aggradation), the contraction-scour value was assumed to be zero in determining the total scour depth (table 1). This assumption was made so that a negative contraction scour would not mask the potentially detrimental effects of local scour at a pier. No abutment scour evaluations were made in this study.



**Table 1.** Cumulative scour depths for the modeled discharges at structure I-465-131-5256 crossing Williams Creek in Hamilton County, Indiana

Pier number <sup>1</sup>	Stationing from bridge plans <sup>2</sup>	Initial bed-elevation at pier (feet)	Main-channel contraction scour depth (feet)	Local scour depth (feet)	Worst-case total-scour depth <sup>3</sup> (feet)	Bottom elevation of pier (feet)	Worst-case bed elevation after scour <sup>4</sup> (feet)
<b>Modeled discharge<sup>5</sup> is 4,300 cubic feet per second</b>							
1	609+09	788	0	6.5	6.5	780.3	779.1
2	609+51	788	0	6.5	6.5	780.4	779.1
<b>Modeled discharge is 7,310 cubic feet per second</b>							
1	609+09	788	2.4	7.4	9.8	780.3	775.8
2	609+51	788	2.4	7.4	9.8	780.4	775.8

<sup>1</sup>Pier numbers were assigned from left to right as shown on the bridge plans.

<sup>2</sup>Stationing is the center line of the pier as determined from the bridge plans. Stationing from bridge plan, 609+09, represents a point 60,909 feet from an arbitrary starting location referenced on the bridge plans.

<sup>3</sup>Worst-case total-scour depths are generated by summing the calculated contraction-scour depth with the worst case of local scour.

<sup>4</sup>Worst-case bed elevation is computed by subtracting the worst-case total-scour depth from the lowest initial bed elevation in the bridge opening (785.6 feet).

<sup>5</sup>Coordinated discharge.

## **SPECIAL CONSIDERATIONS**

Model runs indicate the water-surface elevation at the bridge is lower than the low-steel elevation for the modeled discharges. Therefore, there should be no pressure flow through the bridge opening for the discharges modeled.

## **RESULTS**

Scour depths were computed with a version of WSPRO (Larry Arneson, Federal Highway Administration, written commun., 1996) modified from Shearman (1990). This version of WSPRO includes scour calculations in the model output. Scour depths were calculated assuming an infinite depth of material that could erode and a homogeneous particle-size distribution. The results of the scour analysis are presented in table 1; a complete input file and output results are presented in the appendix.

## **REFERENCES**

- Hoggatt, R.E., 1975, Drainage areas of Indiana streams: U.S. Geological Survey, Water Resources Division, 231 p.
- Indiana State Highway Commission, 1965, Bridge plans Interstate Route 465: Bridge File I-465-131-5256.
- Lagasse, P.F.; Schall, J.D.; Johnson, F.; Richardson, E.V.; and Chang, F., 1995, Stream stability at highway structures (2d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 20, Publication FHWA-IP-90-014, 144 p.
- Richardson, E.V., and Davis, S.R., 1995, Evaluating scour at bridges (3d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 18, Publication FHWA-IP-90-017, 204 p.
- Shearman, J.O., 1990, User's manual for WSPRO, a computer model for water-surface profile computations: Federal Highway Administration Publication FHWA-IP-89-027, 177 p.

## APPENDIX

# WSPRO INPUT FILE

```
T1      I-465 Over Williams Creek  I-465-131-5256
T2      County: Hamilton           Quad: Carmel 111A
T3      4-11-97                    Bret A. Robinson
SI      0
Q       4300
Q       7310
SK      .0025 .0025
XS      EXIT 0 0
GR      60411 820 60538 805 60614 800 60696 795 60809 790 60893 790
GR      60909 789 60915 785.6 60946 785.6 60953 789 61078 795 61193 800
GR      61225 805 61305 820
N       .12 .032 .12
SA      60890 60950
XS      FULLV110 0
GR      60411 820 60538 805 60614 800 60696 795 60809 790 60893 790
GR      60909 789 60915 785.6 60946 785.6 60953 789 61078 795 61193 800
GR      61225 805 61305 820
N       .12 .032 .12
SA      60890 60950
BR      BRDGE110 801 0
GR      60877 0801.2 60877 0800.8 60885 0800.7 60917 0785.7 60945 0785.7
GR      60976 0801.3 60984 0801.3 60984 0801.8 60955 0801.6 60922 0801.5
GR      60890 0801.3 60877 0801.2
N       .035 .032 .035
SA      60900 60970
PD      789 3 1
CD      3 130 2 800.7
*       LXBr RXBr LXApp RXApp * TPierW
DC 0 BRDGE 60889 60972 60910 60960 * 3
DP      60877 60984 2 * * 1 1 1.1
DP      60877 60984 2 * * 1 1 1.1
XS      APPR 370 0
GR      60518 820 60558 815 60592 810 60636 805 60741 800 60809 795
GR      60908 789 60918 785.6 60943 785.6 60952 789 61144 795 61329 800
GR      61486 820
N       .120 .032 .120
SA      60910 60960
EX
ER
```

# WSPRO OUTPUT

\*\*\*\*\* W S P R O \*\*\*\*\*

Federal Highway Administration - U. S. Geological Survey

Model for Water-Surface Profile Computations.

Run Date & Time: 8/ 6/97 10:15 am Version V050196

Input File: 5256.dat Output File: 5256.LST

\*-----\*

T1 I-465 OVER WILLIAMS CREEK I-465-131-5256  
T2 COUNTY: HAMILTON QUAD: CARMEL 111A  
T3 4-11-97 BRET A. ROBINSON  
SI 0  
Q 4300  
Q 7310

\*\*\* Processing Flow Data; Placing Information into Sequence 1 \*\*\*

SK .0025 .0025

\*\*\*\*\* W S P R O \*\*\*\*\*

Federal Highway Administration - U. S. Geological Survey

Model for Water-Surface Profile Computations.

Input Units: English / Output Units: English

\*-----\*

I-465 OVER WILLIAMS CREEK I-465-131-5256  
COUNTY: HAMILTON QUAD: CARMEL 111A  
4-11-97 BRET A. ROBINSON

\*-----\*  
\* Starting To Process Header Record EXIT \*  
\*-----\*

XS EXIT 0 0

GR 60411 820 60538 805 60614 800 60696 795 60809 790 60893 790

GR 60909 789 60915 785.6 60946 785.6 60953 789 61078 795

61193 800

GR 61225 805 61305 820

N .12 .032 .12

SA 60890 60950

\*\*\* Completed Reading Data Associated With Header Record EXIT \*\*\*

\*\*\* Storing X-Section Data In Temporary File As Record Number 1 \*\*\*

\*\*\* Data Summary For Header Record EXIT \*\*\*

SRD Location: 0. Cross-Section Skew: .0 Error Code 0

Valley Slope: .00000 Averaging Conveyance By Geometric Mean.

Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (14 pairs)

X	Y	X	Y	X	Y
60411.000	820.000	60538.000	805.000	60614.000	800.000
60696.000	795.000	60809.000	790.000	60893.000	790.000
60909.000	789.000	60915.000	785.600	60946.000	785.600
60953.000	789.000	61078.000	795.000	61193.000	800.000
61225.000	805.000	61305.000	820.000		

# WSPRO OUTPUT

-----

Minimum and Maximum X,Y-coordinates

Minimum X-Station: 60411.000 ( associated Y-Elevation: 820.000 )  
Maximum X-Station: 61305.000 ( associated Y-Elevation: 820.000 )  
Minimum Y-Elevation: 785.600 ( associated X-Station: 60946.000 )  
Maximum Y-Elevation: 820.000 ( associated X-Station: 60411.000 )

Roughness Data ( 3 SubAreas )

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.120	---
	---	*****
2	.032	---
	---	*****
3	.120	---

-----

\*-----\*

\* Finished Processing Header Record EXIT \*

\*-----\*

\*\*\*\*\* W S P R O \*\*\*\*\*

Federal Highway Administration - U. S. Geological Survey  
Model for Water-Surface Profile Computations.  
Input Units: English / Output Units: English

\*-----\*

I-465 OVER WILLIAMS CREEK I-465-131-5256  
COUNTY: HAMILTON QUAD: CARMEL 111A  
4-11-97 BRET A. ROBINSON

\*-----\*

\* Starting To Process Header Record FULLV \*

\*-----\*

XS FULLV110 0  
GR 60411 820 60538 805 60614 800 60696 795 60809 790 60893 790  
GR 60909 789 60915 785.6 60946 785.6 60953 789 61078 795  
61193 800  
GR 61225 805 61305 820  
N .12 .032 .12  
SA 60890 60950

\*\*\* Completed Reading Data Associated With Header Record FULLV \*\*\*  
\*\*\* Storing X-Section Data In Temporary File As Record Number 2 \*\*\*

\*\*\* Data Summary For Header Record FULLV \*\*\*

SRD Location: 110. Cross-Section Skew: .0 Error Code 0  
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.  
Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (14 pairs)

X	Y	X	Y	X	Y
---	---	---	---	---	---

# WSPRO OUTPUT

60411.000	820.000	60538.000	805.000	60614.000	800.000
60696.000	795.000	60809.000	790.000	60893.000	790.000
60909.000	789.000	60915.000	785.600	60946.000	785.600
60953.000	789.000	61078.000	795.000	61193.000	800.000
61225.000	805.000	61305.000	820.000		

## Minimum and Maximum X,Y-coordinates

Minimum X-Station: 60411.000 ( associated Y-Elevation: 820.000 )  
 Maximum X-Station: 61305.000 ( associated Y-Elevation: 820.000 )  
 Minimum Y-Elevation: 785.600 ( associated X-Station: 60946.000 )  
 Maximum Y-Elevation: 820.000 ( associated X-Station: 60411.000 )

Roughness Data ( 3 SubAreas )		
SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.120	---
	---	*****
2	.032	---
	---	*****
3	.120	---

\*-----\*

\* Finished Processing Header Record FULLV \*

\*-----\*

\*\*\*\*\* W S P R O \*\*\*\*\*

Federal Highway Administration - U. S. Geological Survey

Model for Water-Surface Profile Computations.

Input Units: English / Output Units: English

\*-----\*

I-465 OVER WILLIAMS CREEK I-465-131-5256

COUNTY: HAMILTON QUAD: CARMEL 111A

4-11-97 BRET A. ROBINSON

\*-----\*

\* Starting To Process Header Record BRDGE \*

\*-----\*

BR	BRDGE110	801	0				
GR	60877	0801.2	60877	0800.8	60885	0800.7	60917 0785.7 60945
0785.7							
GR	60976	0801.3	60984	0801.3	60984	0801.8	60955 0801.6 60922
0801.5							
GR	60890	0801.3	60877	0801.2			
N	.035	.032	.035				
SA	60900	60970					
PD	789	3	1				
CD	3	130	2 800.7				

\*\*\* Completed Reading Data Associated With Header Record BRDGE \*\*\*

# WSPRO OUTPUT

+++072 NOTICE: X-coordinate # 2 increased to eliminate vertical segment.  
 +++072 NOTICE: X-coordinate # 8 increased to eliminate vertical segment.  
 \*\*\* Storing Bridge Data In Temporary File As Record Number 3 \*\*\*

\*\*\* Data Summary For Bridge Record BRDGE \*\*\*  
 SRD Location: 110. Cross-Section Skew: .0 Error Code 0  
 Valley Slope: \*\*\*\*\* Averaging Conveyance By Geometric Mean.  
 Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (12 pairs)					
X	Y	X	Y	X	Y
60877.000	801.200	60877.100	800.800	60885.000	800.700
60917.000	785.700	60945.000	785.700	60976.000	801.300
60984.000	801.300	60984.100	801.800	60955.000	801.600
60922.000	801.500	60890.000	801.300	60877.000	801.200

Minimum and Maximum X,Y-coordinates  
 Minimum X-Station: 60877.000 ( associated Y-Elevation: 801.200 )  
 Maximum X-Station: 60984.100 ( associated Y-Elevation: 801.800 )  
 Minimum Y-Elevation: 785.700 ( associated X-Station: 60945.000 )  
 Maximum Y-Elevation: 801.800 ( associated X-Station: 60984.100 )

Roughness Data ( 3 SubAreas )		
SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.035	---
	---	*****
2	.032	---
	---	*****
3	.035	---

Discharge coefficient parameters				
BRTYPE	BRWdth	EMBSS	EMBElv	UserCD
3	130.000	2.00	800.700	*****

Pressure flow elevations	
AVBCEL	PFElev
*****	801.000

Abutment Parameters					
ABSLPL	ABSLPR	XTOELT	YTOELT	XTOERT	YTOERT
*****	*****	*****	*****	*****	*****

Pier/Pile Data ( 1 Group(s) )			
Code Indicates Bridge Uses Piers			
Group	Elevation	Gross Width	Number
1	789.000	3.000	1



# WSPRO OUTPUT

```
*-----*
*      Finished Processing Header Record BRDGE      *
*-----*
```

```
***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English
```

```
*-----*
I-465 OVER WILLIAMS CREEK I-465-131-5256
COUNTY: HAMILTON QUAD: CARMEL 111A
4-11-97 BRET A. ROBINSON
DC 0 BRDGE 60889 60972 60910 60960 * 3
DP 60877 60984 2 * * 1 1 1.1
DP 60877 60984 2 * * 1 1 1.1
```

```
*-----*
*      Starting To Process Header Record APPR      *
*-----*
```

```
XS APPR 370 0
GR 60518 820 60558 815 60592 810 60636 805 60741 800 60809 795
GR 60908 789 60918 785.6 60943 785.6 60952 789 61144 795
61329 800
GR 61486 820
N .120 .032 .120
SA 60910 60960
```

```
*** Completed Reading Data Associated With Header Record APPR ***
*** Storing X-Section Data In Temporary File As Record Number 4 ***
```

```
*** Data Summary For Header Record APPR ***
SRD Location: 370. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00
```

X,Y-coordinates (13 pairs)					
X	Y	X	Y	X	Y
60518.000	820.000	60558.000	815.000	60592.000	810.000
60636.000	805.000	60741.000	800.000	60809.000	795.000
60908.000	789.000	60918.000	785.600	60943.000	785.600
60952.000	789.000	61144.000	795.000	61329.000	800.000
61486.000	820.000				

```
Minimum and Maximum X,Y-coordinates
Minimum X-Station: 60518.000 ( associated Y-Elevation: 820.000 )
Maximum X-Station: 61486.000 ( associated Y-Elevation: 820.000 )
Minimum Y-Elevation: 785.600 ( associated X-Station: 60943.000 )
Maximum Y-Elevation: 820.000 ( associated X-Station: 60518.000 )
```

Roughness Data ( 3 SubAreas )

# WSPRO OUTPUT

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.120	---
	---	*****
2	.032	---
	---	*****
3	.120	---

Bridge datum projection(s): XREFLT XREFRT FDSTLT FDSTRT  
\*\*\*\*\*

\*-----\*  
\* Finished Processing Header Record APPR \*  
\*-----\*

\*\*\*\*\* W S P R O \*\*\*\*\*  
Federal Highway Administration - U. S. Geological Survey  
Model for Water-Surface Profile Computations.  
Input Units: English / Output Units: English  
\*-----\*  
I-465 OVER WILLIAMS CREEK I-465-131-5256  
COUNTY: HAMILTON QUAD: CARMEL 111A  
4-11-97 BRET A. ROBINSON

EX

\*=====\*

\* Summary of Boundary Condition Information \*

\*=====\*

#	Reach Discharge	Water Surface Elevation	Friction Slope	Flow Regime
1	4300.00	*****	.0025	Sub-Critical
2	7310.00	*****	.0025	Sub-Critical

\*=====\*

\* Beginning 2 Profile Calculation(s) \*

\*=====\*

\*\*\*\*\* W S P R O \*\*\*\*\*  
Federal Highway Administration - U. S. Geological Survey  
Model for Water-Surface Profile Computations.  
Input Units: English / Output Units: English  
\*-----\*  
I-465 OVER WILLIAMS CREEK I-465-131-5256  
COUNTY: HAMILTON QUAD: CARMEL 111A  
4-11-97 BRET A. ROBINSON

WSEL	VHD	Q	AREA	SRDL	LEW
EGEL	HF	V	K	FLEN	REW

# WSPRO OUTPUT

	CRWS	HO	FR #	SF	ALPHA	ERR
Section: EXIT	793.921	.831	4300.000	1170.048	*****	60720.390
Header Type: XS	794.752	*****	3.675	85978.46	*****	61055.520
SRD: .000	792.407	*****	.690	*****	3.958	*****

Section: FULLV	794.300	.702	4300.000	1300.384	110.000	60711.810
Header Type: FV	795.003	.246	3.307	96044.64	110.000	61063.430
SRD: 110.000	792.407	.000	.616	.0022	4.129	.004

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

Section: APPR	794.737	.902	4300.000	1167.780	260.000	60813.340
Header Type: AS	795.639	.539	3.682	92877.37	260.000	61135.570
SRD: 370.000	792.857	.100	.705	.0021	4.279	-.003

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>>

<<< Beginning Bridge/Culvert Hydraulic Computations >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: BRDGE	793.773	2.283	4300.000	360.323	110.000	60899.780
Header Type: BR	796.056	.468	11.934	52550.45	110.000	60961.040
SRD: 110.000	793.289	.833	.881	*****	1.031	-.003

Specific Bridge Information	C	P/A	PFELEV	BLEN	XLAB	XRAB
Bridge Type 3	Flow Type 1					
Pier/Pile Code 0	.9850	.040	801.000	*****	*****	*****

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: APPR	796.974	.388	4300.000	2014.247	130.000	60782.150
Header Type: AS	797.362	.314	2.135	157406.60	134.585	61217.040
SRD: 370.000	792.857	.997	.409	.0021	5.479	.018

Approach Section APPR Flow Contraction Information						
M( G )	M( K )	KQ	XLKQ	XRKQ	OTEL	
.803	.264	115326.0	*****	*****	796.974	

<<< End of Bridge Hydraulics Computations >>>

\*\*\*\*\* W S P R O \*\*\*\*\*  
Federal Highway Administration - U. S. Geological Survey

# WSPRO OUTPUT

Model for Water-Surface Profile Computations.  
Input Units: English / Output Units: English

\*-----\*

I-465 OVER WILLIAMS CREEK I-465-131-5256  
COUNTY: HAMILTON QUAD: CARMEL 111A  
4-11-97 BRET A. ROBINSON

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: EXIT	795.913	1.060	7310.000	1922.222	*****	60681.020
Header Type: XS	796.973	*****	3.803	146110.30	*****	61099.000
SRD: .000	794.088	*****	.679	*****	4.713	*****
Section: FULLV	796.292	.923	7310.000	2083.619	110.000	60674.800
Header Type: FV	797.216	.252	3.508	159631.80	110.000	61107.730
SRD: 110.000	794.088	.000	.619	.0023	4.822	-.010

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

Section: APPR	796.721	1.227	7310.000	1905.638	260.000	60785.600
Header Type: AS	797.948	.584	3.836	149006.90	260.000	61207.660
SRD: 370.000	794.869	.152	.737	.0022	5.362	-.004

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>>

<<< Beginning Bridge/Culvert Hydraulic Computations >>>

==210 QUESTIONABLE CRITICAL-FLOW SOLUTION AT SECID "BRDGE".

Q, CRWS: 7310.00 795.87

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: BRDGE	795.869	3.921	7310.000	497.749	110.000	60895.310
Header Type: BR	799.789	*****	14.686	84705.07	110.000	60965.210
SRD: 110.000	795.869	*****	1.049	*****	1.169	*****

Specific Bridge Information	C	P/A	PFELEV	BLN	XLAB	XRAB
Bridge Type 3 Flow Type 1						
Pier/Pile Code 0	.9250	.041	801.000	*****	*****	*****

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: APPR	800.786	.336	7310.000	4032.697	130.000	60724.500
Header Type: AS	801.122	.279	1.813	323338.70	137.181	61335.170
SRD: 370.000	794.869	1.054	.319	.0022	6.576	.004

# WSPRO OUTPUT

Approach M( G )	Section M( K )	APPR KQ	Flow XLKQ	Contraction XRKQ	Information OTEL
.830	.373	202662.2	*****	*****	800.786

<<< End of Bridge Hydraulics Computations >>>

\*\*\*\*\* W S P R O \*\*\*\*\*

Federal Highway Administration - U. S. Geological Survey  
Model for Water-Surface Profile Computations.  
Input Units: English / Output Units: English

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I-465 OVER WILLIAMS CREEK I-465-131-5256  
COUNTY: HAMILTON QUAD: CARMEL 111A  
4-11-97 BRET A. ROBINSON

\*\*\* Live-Bed Contraction Scour Calculations for Header Record BRDGE \*\*\*

## Constants and Input Variables

\*-----\*

Bed Material Transport Mode Factor (k1):	.64
Total Pier Width Value (Pw):	3.000

\*-----\*

#	Scour Depth	-- Flow -- Contract	-- Width -- Approach	-- X-Limits -- Contract	-- Approach
1	-.066	4300.000	3042.667	80.000	50.000
	.....	Approach Channel Depth:	10.287	.....	Right:
*	Negative Scour Depth Encountered - Check If Variables Are Reasonable *				
2	2.432	7310.000	4258.095	80.000	50.000
	.....	Approach Channel Depth:	14.098	.....	Right:

\*\*\*\*\* W S P R O \*\*\*\*\*

Federal Highway Administration - U. S. Geological Survey  
Model for Water-Surface Profile Computations.  
Input Units: English / Output Units: English

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I-465 OVER WILLIAMS CREEK I-465-131-5256  
COUNTY: HAMILTON QUAD: CARMEL 111A  
4-11-97 BRET A. ROBINSON

\*\*\* Pier Scour Calculations for Header Record BRDGE \*\*\*

## Constants and Input Variables

Pier Width: 2.000

\*-----\*

# WSPRO OUTPUT

```

Pier Shape Factor          (K1):  1.00
Flow Angle of Attack Factor (K2):  1.00
Bed Condition Factor        (K3):  1.10
Bed Material Factor         (K4):  1.00
Velocity Multiplier         (VM):  1.00
Depth Multiplier            (YM):  1.00

```

\*-----\*

#	Scour Depth	---- Localized Hydraulic Properties ----					-- X-Stations --	
		Flow	WSE	Depth	Velocity	Froude #	Left	Right
1	6.49	4300.000	794.770	9.070	12.334	.722	60877.000	60984.000
2	7.39	7310.000	796.922	11.222	15.614	.821	60877.000	60984.000

\*\*\*\*\* W S P R O \*\*\*\*\*

Federal Highway Administration - U. S. Geological Survey

Model for Water-Surface Profile Computations.

Input Units: English / Output Units: English

\*-----\*

```

I-465 OVER WILLIAMS CREEK I-465-131-5256
COUNTY: HAMILTON        QUAD: CARMEL 111A
4-11-97                  BRET A. ROBINSON

```

\*\*\* Pier Scour Calculations for Header Record BRDGE \*\*\*

Constants and Input Variables

Pier Width: 2.000

\*-----\*

```

Pier Shape Factor          (K1):  1.00
Flow Angle of Attack Factor (K2):  1.00
Bed Condition Factor        (K3):  1.10
Bed Material Factor         (K4):  1.00
Velocity Multiplier         (VM):  1.00
Depth Multiplier            (YM):  1.00

```

\*-----\*

#	Scour Depth	---- Localized Hydraulic Properties ----					-- X-Stations --	
		Flow	WSE	Depth	Velocity	Froude #	Left	Right
1	6.49	4300.000	794.770	9.070	12.334	.722	60877.000	60984.000
2	7.39	7310.000	796.922	11.222	15.614	.821	60877.000	60984.000

ER

\*\*\*\*\* Normal end of WSPRO execution. \*\*\*\*\*

\*\*\*\*\* Elapsed Time: 0 Minutes 4 Seconds \*\*\*\*\*